# BROWARD COUNTY GO SOLAR BROWARD COUNTY ENVIRONMENTAL PLANNING AND GROWTH MANAGEMENT DEPARTMENT

## BROWARD ROOFTOP SOLAR PHOTOVOLTAIC ROOFTOP MOUNTING SYSTEMS



#### **DRAWING INDEX**

COV COVER

#### **ARCHITECTURAL**

A1 PLAN VIEW A2 SECTION

A3 SECTIONS

A4 CALCULATIONS

A5 WATERPROOFING DETAILS

### CARTAYA & ASSOCIATES ARCHITECTS, P.A.

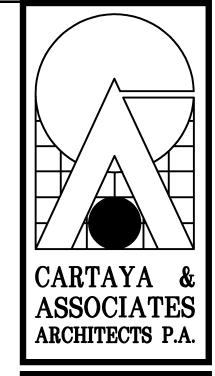
3077 E. COMMERCIAL BLVD. SUITE 201 FT. LAUDERDALE, FL. 33308 954-771-2724

(ARCHTECTURE)

### TY LIN INTERNATIONAL, INC.

201 ALHAMBRA CIRCLE, SUITE 900 CORAL GABLE, FL. 33134 305-567-1888

(STRUCTURAL/M.E.P./ENGINEERING)



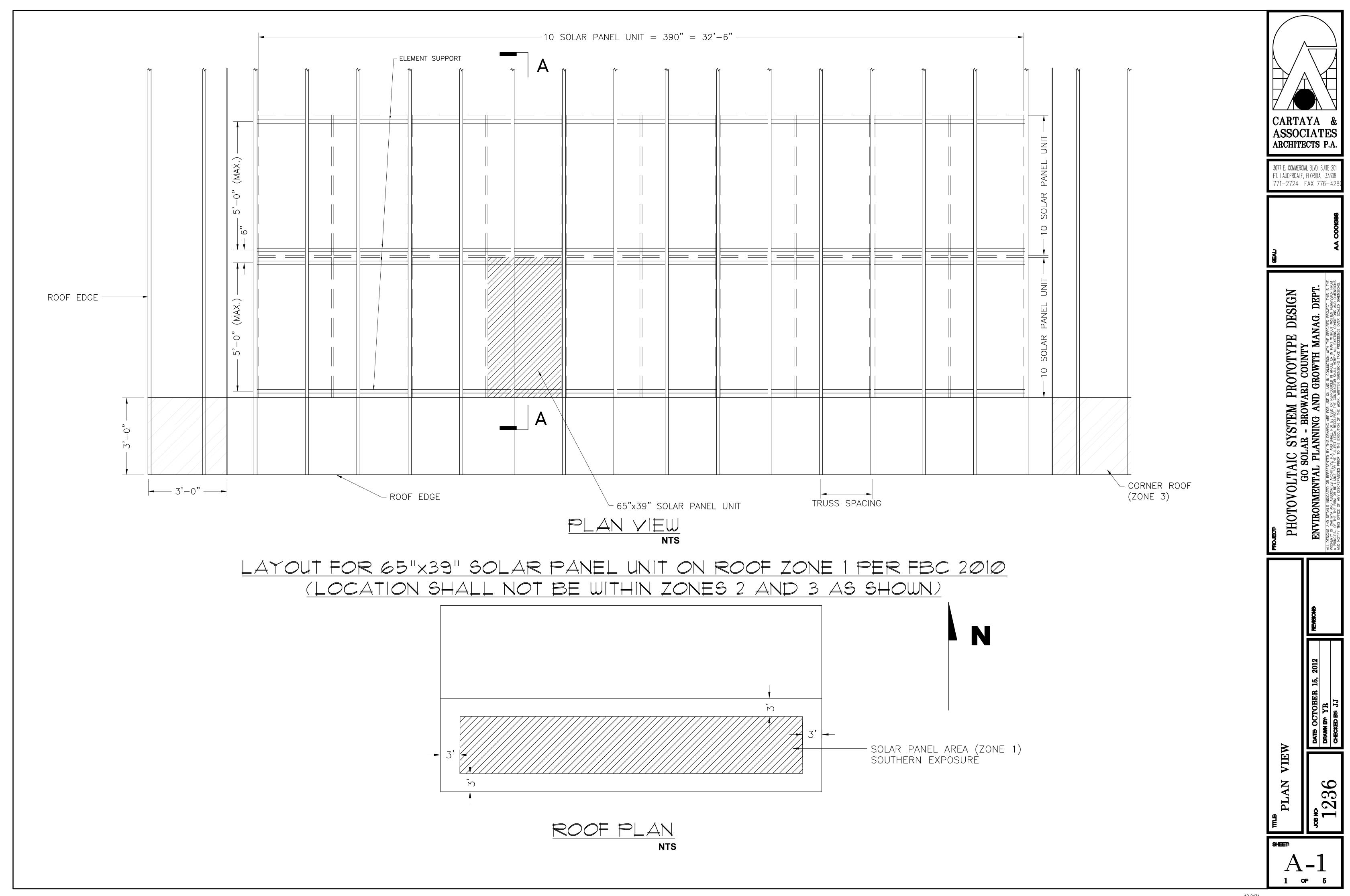
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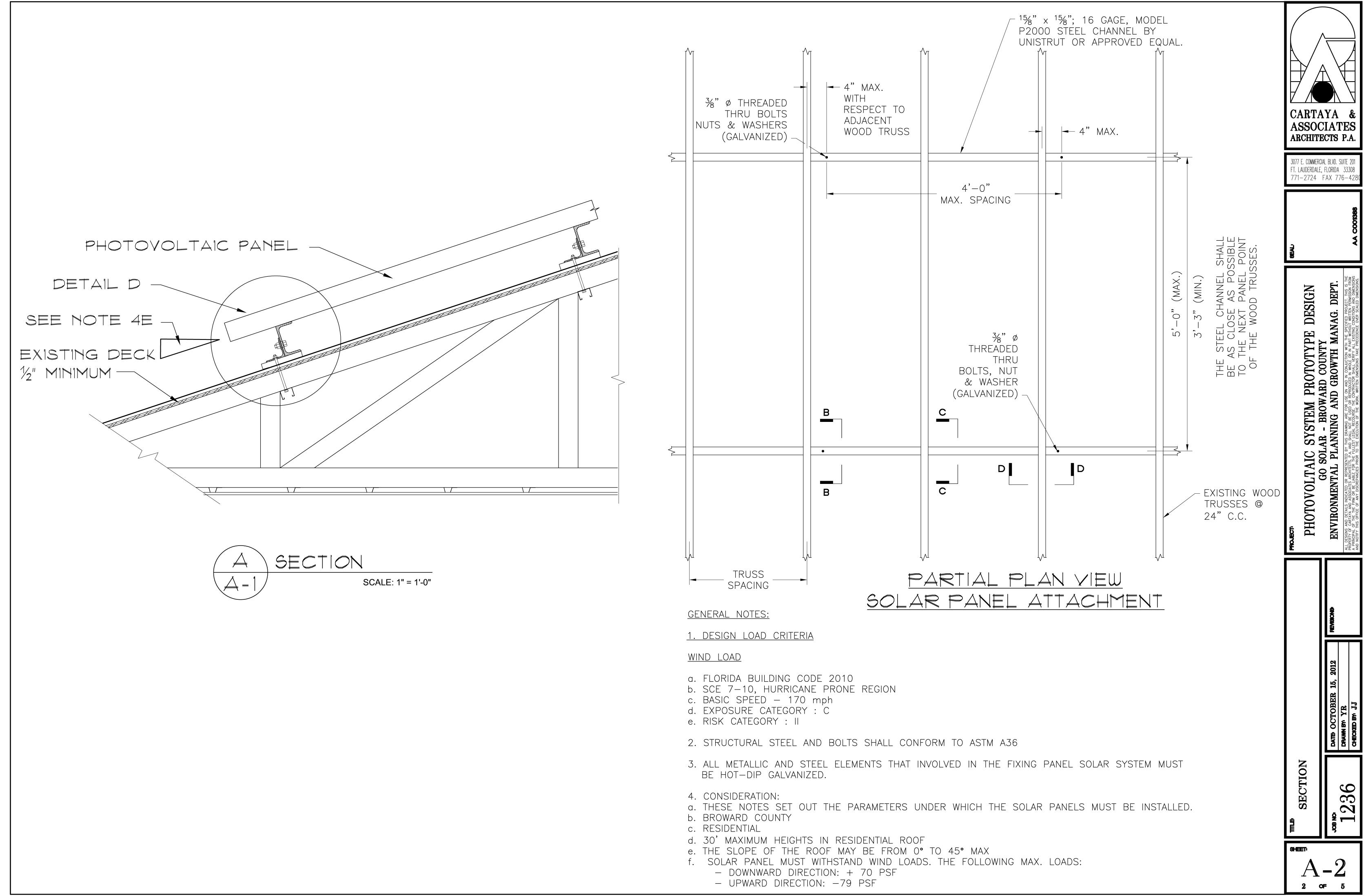
PHOTOVOLTAIC SYSTEM PROTOTYPE DESIGN
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ENVIRONMENTAL PLANNING AND GROWTH MANAG. DEPT

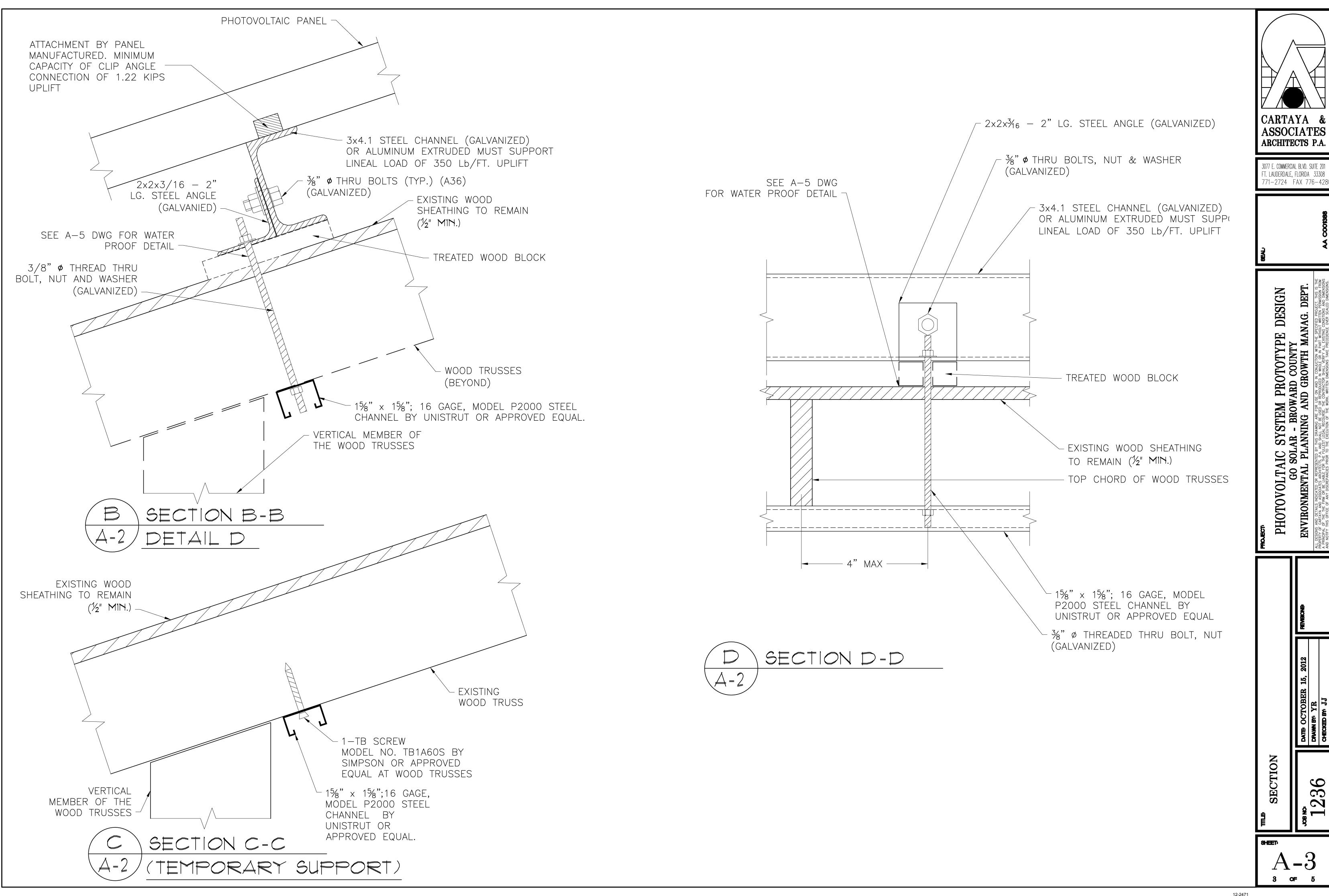
HEET

DATE OCTOBER 15, 2012

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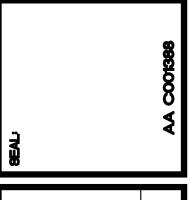








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PHOTOVOLTAIC SYSTEM PROTOTYPE DESIGN
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DATE OCTOBER 10, 2012
DRAWN BY YR
CHECKED BY JJ

CALCS

SHEET:

A - 4

4 OF 5

WIND LOAD PRESSURE

Using Rooftop Structures and Equipments (29.5.1 Sheet 308) Broward County

Residential: || risk category. (Table 1.5.1/ Sheet 2)

V= 170 Mph

K<sub>d</sub>= 0.85 (Table 26.6-1/ Sheet 250) K<sub>d</sub>= 1.0

 $Z=15' \rightarrow K_{s}=0.85$  (Table 29.3-1/ Sheet 310)

 $Z = 20^{\circ} \rightarrow K_{x} = 0.90$ 

 $Z=25' \rightarrow K_{g}=0.94$ 

 $Z=30' \rightarrow K_s=0.98$ 

 $Q = 0.00256 K_1 \times K_2 \times K_3 \times V^2$ 

 $q_{25} = 53.4 \, lb/ft^2$ 

q<sub>20</sub> = 56.6 lb/ft<sup>2</sup>

q<sub>25</sub> = 59.1 lb/ft<sup>2</sup>

 $q_{xy} = 61.6 \text{ lb/ft}^2$ 

Note:

- 1- We use zone 2 for the calculation of wind load, assuming that the panels may be installed in zone 1 and 2.
- 2- We consider that the panels are part of the roof and  $GC_{st} = \pm 0.18$  (Worst Condition)

0s7° (Gable Roof) Fig 30.A-2A/ Sheet 336

 $GC_{p123} = +0.3$ 

 $GC_{n2} = -1.8$  (This coefficient value is the most critical for the upward load.)

7°<8527° (Gable/ Hip Roof) Fig 30.4-28/ Sheet 337)

 $GC_{p123} = +0.5$ 

GC<sub>p2</sub> = -1.7

27°<6≤45° (Gables Roof) Fig 30.4-2C/ Sheet 338

 $GC_{p123} = +0.9$  (This coefficient value is the most critical for the downward load.)

GC<sub>p3</sub> = -1.2

 $\mathbf{P} = \mathbf{q}_n \left[ \left( \mathbf{G} \mathbf{C}_p \right) - \left( \mathbf{G} \mathbf{C}_p \right) \right]$ 

27°<0s45° h = 30′

 $p_{123} = 61.6[0.9-(-0.18)] = +66.5 lb/ft^2$  (Downward Pressure)

057° h = 30°

 $p_2 = 61.6[-1.8-(+0.180] = 122 |b/ft^2|$  (Upward Pressure)

27°<6≤45° (Monoslope roof) Fig 30.4-5A/ Sheet 341

 $GC_{p223} = +0.3$ 

GC<sub>p2</sub> = -1.7

CONNECTION DESIGN

Panel Point Spacing 5'-0" Max

Uplift @ Connect

 $F = 122 \frac{lb}{ft^2} \times \frac{5"}{2} \times 4' = 1220 \, lb/Connection/Upward$ 

4': Max Spacing Anchor

Steel Channel Design

$$M = \frac{F \times a \times b}{l} = \frac{1.22 \times 0.33 \times 1.66'}{2'} = 0.334 \text{ k. ft}$$

$$S_{Req} = \frac{M}{0.6F_y} = \frac{0.334 \times 1.2^y}{0.6 \times 36} = 0.016 n^3 < 0.072 \, n^3 \rightarrow \text{Steel Channel 1}^5/8^x \times \frac{7}{8}^x \times 12 \text{gauge S=0.072} n^3 = 0.037 n^4$$

Model No. P3300

#### Steel Track Design

$$W = \frac{122lb}{ft^2} \times \frac{5'}{2} = 305 \, lb/ft$$

$$\Delta = \frac{L}{360} = \frac{4' \times 12''}{360} 0.1333''$$

$$I = \frac{5 \times wl^4 \times 1728}{384 \times 29000 \times \Delta} = \frac{5 \times 0.305 \times 4^4 \times 1728}{384 \times 29000 \times 0.1333} = I = 0.46n^4$$

Use: [ 3x4.1 Steel Channel (!= 1.66n\*, S= 1.10 n\*)

#### Steel Bolt Anchor Design

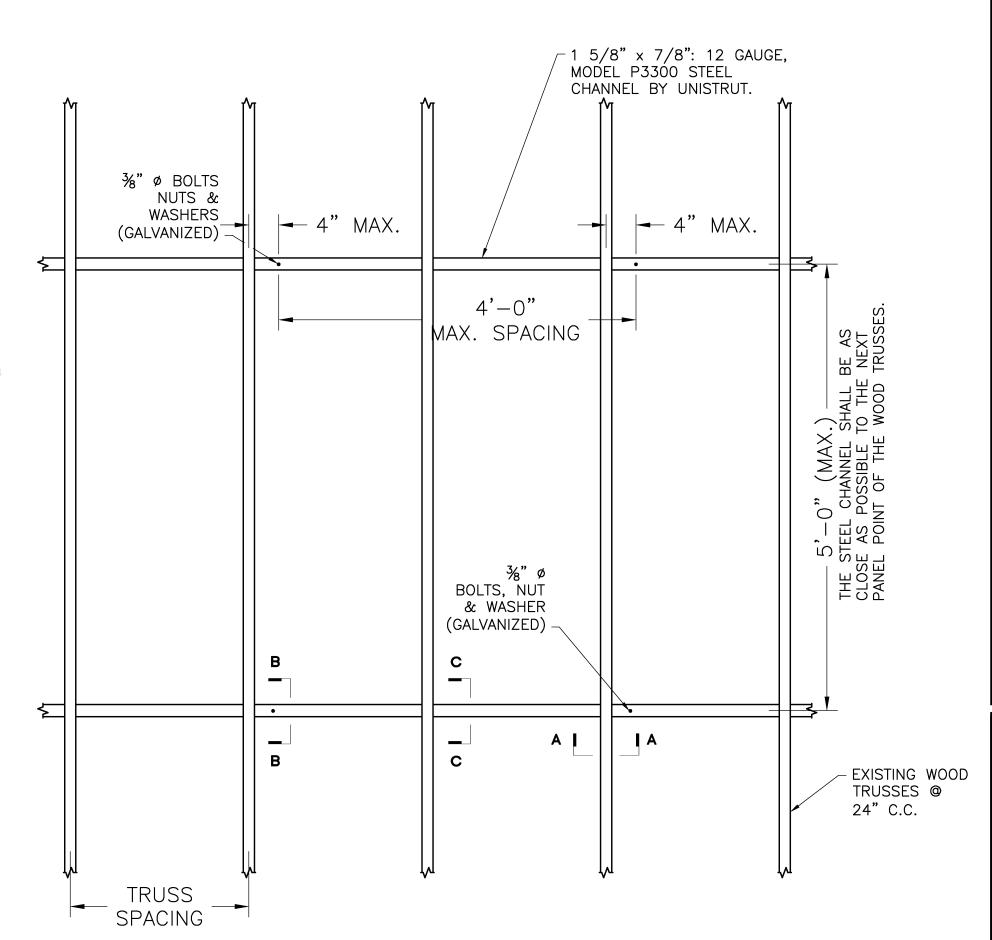
F= 1..22k Tension

 $3/8^{\circ}$   $\Phi$  area =  $\pi R^2 = 0.1104 n^2$ 

For A36 Bolt  $\rightarrow$  F<sub>0</sub>= 58 k/n<sup>2</sup>

F<sub>t</sub>= 0.33F<sub>s</sub>= 19.14 k/n<sup>2</sup>

 $F_{Alloward} = A \times F_t = 0.1104 \times 19.14 \text{ k/n}^2 = 2.1^k > 1.22^k \text{ (Tension)} OK$ 



SOLAR PANEL ATTACHMENT PLAN VIEW

